

providing insights for today's hvac system designer

# Engineers Newsletter

volume 39-4

## Effects of Altitude on psychrometric calculations and fan selections

For this EN we're pulling from the archives to address a subject that still causes confusion within the industry and continues to be the subject of frequently asked questions. This EN investigates the effects of altitude on psychrometric calculations and fan selections.

### "Standard Air"

As altitude increases, the average barometric pressure drops and air density decreases.

"Standard air" has historically been defined by ASHRAE as having a density of 0.075 lb/ft<sup>3</sup>, which equates to air density at sea level (barometric pressure of 29.92 in. Hg). The 2009 *ASHRAE Handbook of Fundamentals* (page 18.13) states that this condition is represented by either saturated air at 60°F dry bulb or dry air at 69°F dry bulb.

Since the performance of heating, cooling, and air-moving equipment is commonly rated at "standard air" conditions, cataloged performance data cannot be used directly for higher altitude applications. For instance, at a barometric pressure of 24 in. Hg (approximately 6000 ft altitude), cataloged data may be off by as much as 20 to 40 percent.

While areas above 6000 ft are statistically limited, a number of states and cities have barometric pressures in the range of 29 to 27 in.

Hg. In this range, cataloged ratings may differ from actual conditions by 3 to 20 percent.

### Psychrometric Calculations

The equations used in psychrometric calculations remain the same for all altitudes. However, some of the factors used in these equations are affected by altitude.

The sensible heat gain ( $Q_s$ ) equation is often displayed as follows:

$$Q_s = 1.085 \times \text{cfm} \times \Delta T$$

However, the 1.085 in this equation is not a constant. Rather, it is the product of the density ( $\rho$ ) and specific heat ( $C_p$ ) of the air at "standard air" conditions, and the conversion factor of 60 minutes per hour.

$$Q_s = (\rho \times C_p \times 60 \text{ min/hr}) \times \text{cfm} \times \Delta T$$

The specific heat for 69°F dry air at sea level is 0.241 Btu/lb°F. Therefore, at "standard air" conditions, these properties result in the value 1.085.

$$0.075 \text{ lb/ft}^3 \times 0.241 \text{ Btu/lb}^\circ\text{F} \times 60 \text{ min/hr} \\ = 1.085$$

The latent heat gain ( $Q_L$ ) equation is often displayed as follows:

$$Q_L = 0.69 \times \text{cfm} \times \Delta W \text{ (gr/lb)}$$

However, the 0.69 in this equation is not a constant. Rather, it is the product of the density and latent heat of vaporization ( $\Delta h_{\text{vap}}$ ) of the air at "standard air" conditions, and the conversion factors of 60 minutes per hour and 7000 grains/lb.

$$Q_L = (\rho \times \Delta h_{\text{vap}} \times 60 \text{ min/hr} / 7000 \text{ gr/lb}) \times \text{cfm} \times \Delta W$$

The latent heat of vaporization for 69°F dry air at sea level is 1076 Btu/lb. Therefore, at "standard air" conditions, these properties result in the value 0.69.

$$(0.075 \text{ lb/ft}^3 \times 1076 \text{ Btu/lb} \times 60 \text{ min/hr}) / 7000 \text{ gr/lb} = 0.69$$

The total heat gain ( $Q_T$ ) equation is often displayed as follows:

$$Q_T = 4.5 \times \text{cfm} \times \Delta h$$

However, the 4.5 in this equation is not a constant. Rather, it is the product of the density of the air at "standard air" conditions and the conversion factor of 60 minutes per hour.

$$Q_T = (\rho \times 60 \text{ min/hr}) \times \text{cfm} \times \Delta h$$

For "standard air" density, the result is the value 4.5.

$$0.075 \text{ lb/ft}^3 \times 60 \text{ min/hr} = 4.5$$

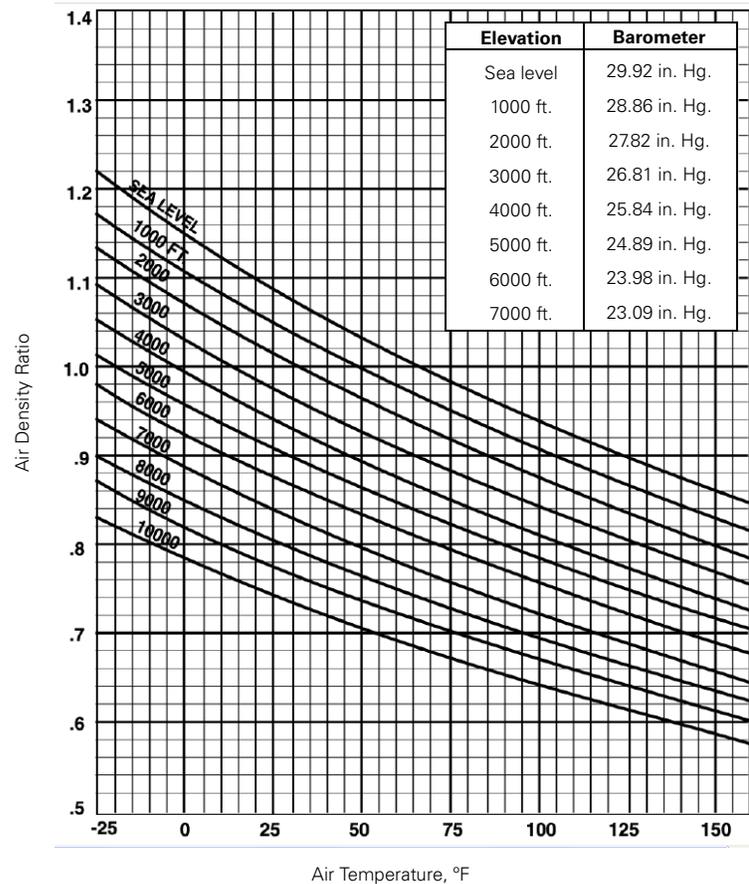
Air at other conditions and other altitudes will cause these factors to change.

## Fans

Fans are considered to be constant-volume devices. That is, a given fan will deliver a specific volumetric flow rate (cfm) at a specific fan rotational speed (rpm). The mass of air that the fan moves at a given speed will vary based on the density of the air being moved. Air density also changes the static pressure that the fan will develop and the horsepower needed to drive it.

Fan and air handler manufacturers typically catalog fan performance data at "standard air" conditions. If the airflow requirement for a given

Figure 1. Air density ratios



application is stated at non-standard conditions, a density correction must be made prior to selecting a fan.

The procedure for selecting a fan at actual altitude (or temperatures) is outlined in the following steps:

- 1 Determine the actual air density and calculate the air density ratio, which is the density at actual conditions divided by density at standard conditions. Figure 1 provides a useful chart for determining the air density ratio based on altitude and air temperature.
- 3 Use the actual design airflow (cfm) and the static pressure corrected for standard conditions (see Step 2) to select the fan from the performance tables/charts and to determine the speed (rpm) and horsepower requirement of the fan at standard conditions.
- 4 The fan speed (rpm) is the same at both actual and standard conditions.

$$\text{RPM}_{\text{actual}} = \text{RPM}_{\text{standard}}$$

- 5 Multiply the input power requirement by the air density ratio to determine the actual input power required.

$$\text{Power}_{\text{actual}} = \text{Air Density Ratio} \times \text{Power}_{\text{standard}}$$

$$\text{Air Density Ratio} = \frac{\text{Density}_{\text{actual}}}{\text{Density}_{\text{standard}}}$$

- 2 Divide the design static pressure at actual conditions by the air density ratio determined in Step 1.

$$\text{SP}_{\text{standard}} = \frac{\text{SP}_{\text{actual}}}{\text{Air Density Ratio}}$$

It is important to note that most pressure-loss charts for other system components (such as ducts, filters, coils, and dampers) are also based on standard air conditions.

---

## Summary

Although the wide-scale use of computer software to select HVAC equipment has made the process of correcting for altitude simpler, a fundamental understanding is still important to prevent mistakes and troubleshoot problems.

By Trane Applications Engineering. You can find this and previous issues of the Engineers Newsletter at [www.trane.com/engineersnewsletter](http://www.trane.com/engineersnewsletter). To comment, e-mail us at [comfort@trane.com](mailto:comfort@trane.com).

---

## View the latest on-demand courses:

**ASHRAE Standard 90.1-2010.**

**Energy-Saving Strategies for Rooftop VAV Systems.**

**ASHRAE Standard 62.1: Ventilation Rate Procedure.**

**LEED 2009 Modeling and Energy Savings.**

The courses were developed and are offered free of charge to demonstrate Trane's commitment to sustainable design. LEED Accredited Professionals (APs) and AIA members can participate and earn an average of 1.5 Continuing Education (CE) hours per program.

Visit [www.trane.com/continuingeducation](http://www.trane.com/continuingeducation) to view all current courses and details.

---

## New application manuals now available

**Central Geothermal Design and Control.** (SYS-APM009-EN, April 2010)

**Chilled-Water VAV Systems.** (SYS-APM008-EN, August 2009)

**Chiller System Design and Control.** (SYS-APM001-EN, May 2009)

Visit [www.trane.com/bookstore](http://www.trane.com/bookstore) to order and view a complete list of resources.

# Engineers Newsletter **LIVE!**

*To register, contact your  
local Trane office.*

**March 2011  
Upgrading Existing  
Chilled-Water  
Systems**

**June 2011  
High-Performance  
VAV Systems**

**October 2011  
Dedicated  
Outdoor Air Units**



*Trane,  
A business of Ingersoll Rand*

*For more information, contact your local Trane  
office or e-mail us at [comfort@trane.com](mailto:comfort@trane.com)*

Trane believes the facts and suggestions presented here to be accurate. However, final design and application decisions are your responsibility. Trane disclaims any responsibility for actions taken on the material presented.